



Fig. 12.8 Idealized structure for wind load design.

- Windward side

$$\text{permanent} + \text{variable} = 1G_{kj} - 1.5 W_{ki}$$

$$\text{stress} = \frac{1 \times 168.08}{102.5} - 1.5 \times 4.96 = 1.64 - 0.744$$

$$= 0.896 \text{ N/mm}^2 \quad (\text{no tension})$$

- Leeward side

$$\text{permanent} + \text{variable} = 1.35 G_{kj} + 1.5 W_{ki}$$

$$\text{stress} = 2.2 + 0.744 = 2.944 \text{ N/mm}^2$$

$$\text{permanent} + \text{all variable actions} = 1.35 G_{kj} + 1.35 Q_{ki} \pm 1.35 W_{ki}$$

$$\text{stress} = \frac{1.35 \times 168.08}{102.5} + \frac{1.35 \times 22.68}{102.5}$$

$$\pm 1.35 \times 0.496$$

$$= 2.20 + 0.3 \pm 0.67$$

$$= 3.17 \text{ or } 1.83 \text{ N/mm}^2 \quad (\text{no tension})$$

Hence, most unfavourable action is $1.35G_{kj}+1.35Q_{ki}+1.35 W_{ki}$ and the design load= $3.17 \times 102.5 \times 10^3 / 10^3 = 324.9 \text{ kN/m}$.

12.7.1 Selection of brick and mortar combination for wall A: according to EC6

Design vertical load resistance of wall $N_{Rd} = \phi_{i,m} t f_k / \gamma_{m'}$, where $\phi_{i,m}$ depends on eccentricity and slenderness ratio $SR = \frac{3}{4} \times 2.85 / 102.5 \times 10^3 = 20.85$.

12.7.2 Calculation of eccentricity

Figure 12.9 shows the worst combination of loading for obtaining the value of eccentricity. Axial load

$$P = 1 \times 143.40 + 1.5 \times 19.44$$

$$= 172.56 \text{ kN}$$

$$P_1 = 1.35 \times 4.8 \times 1.2 \times 1.5 + 1.5 \times 2.7$$

$$= 11.66 + 4.05$$

$$= 15.71 \text{ kN}$$

$$P_2 = 1.35 \times G_k = 11.66 \text{ kN}$$